Angular Momentum Presentation Week 2

from Iskenderian and Salstein, Monthly Weather Review (1998)

2. Definitions and data sources

The global atmospheric angular momentum about the earth's axis can be expressed as

$$AAM = M_r + M_{\Omega}, \tag{1}$$

where

$$M_r = \frac{a^3}{g} \iiint u \cos^2 \phi \ d\phi \ d\lambda \ dp \tag{2}$$

is the entire atmosphere's angular momentum associated with its motion relative to the rotating solid earth, a is the earth's radius, g is acceleration due to gravity, u is zonal wind, and the integral is performed over all latitudes ϕ , longitudes λ , and pressures p. The angular mo-

mentum associated with the rotation of the atmosphere's mass is

$$M_{\Omega} = \frac{a^4 \Omega}{g} \int \int p_s \cos^3 \phi \ d\phi \ d\lambda, \tag{3}$$

where Ω is the mean rotation rate of the earth and p_s the surface pressure (Rosen 1993).

The conservation of angular momentum states that changes in AAM are related to the surface torque by the relationship

$$\frac{d}{dt}AAM = T_m + T_f, \tag{4}$$

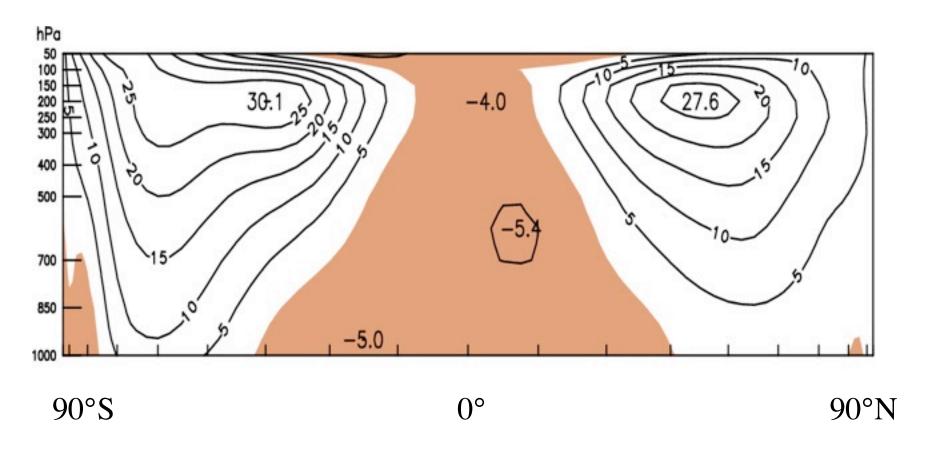
where the mountain torque (T_m) and friction torque (T_f) are defined through the following relationships (White 1991):

$$T_m = -a^2 \int \int p_s \frac{\partial H}{\partial \lambda} \cos \phi \ d\phi \ d\lambda, \tag{5}$$

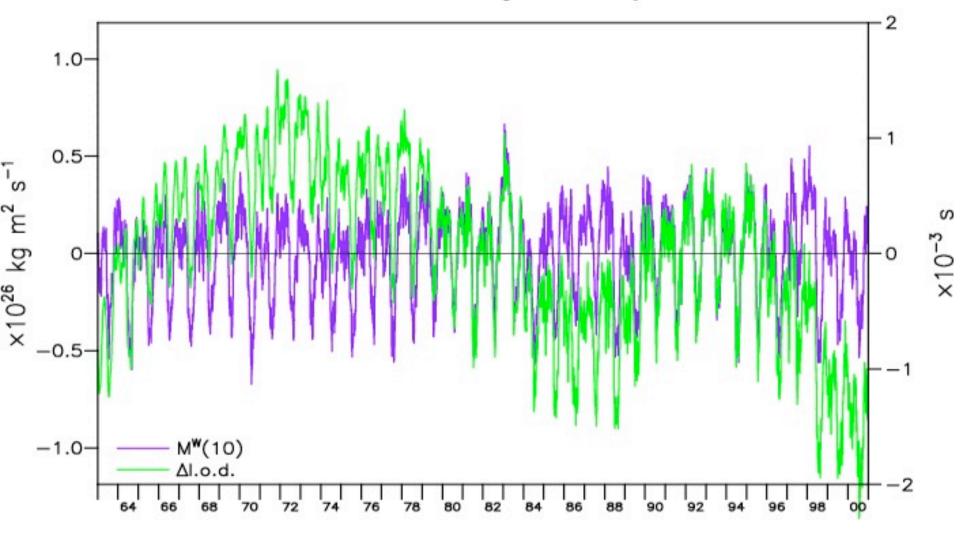
$$T_f = a^3 \int \int \tau \cos^2 \phi \ d\phi \ d\lambda. \tag{6}$$

Here, τ is surface stress and H indicates the height of the sloping topography.

zonally averaged zonal wind [u] (m s⁻¹)



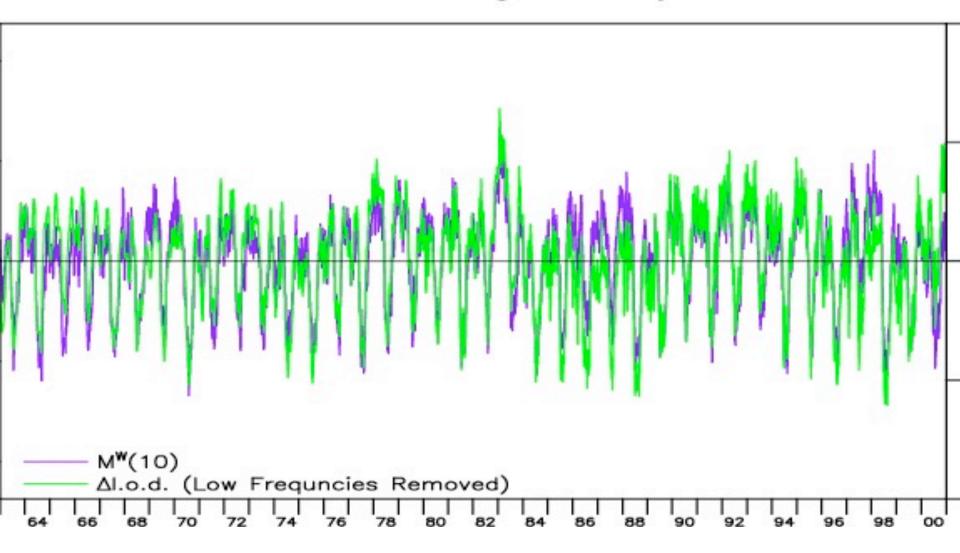
AAM and Length of Day



$$\Delta M = k \times \Delta(L.O.D.)$$

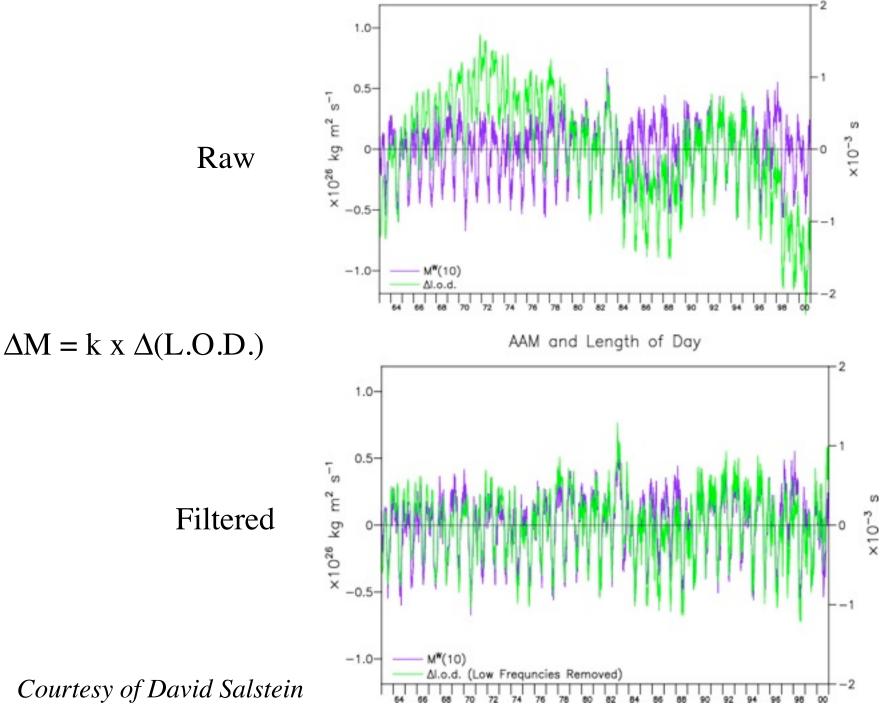
Courtesy of David Salstein

AAM and Length of Day

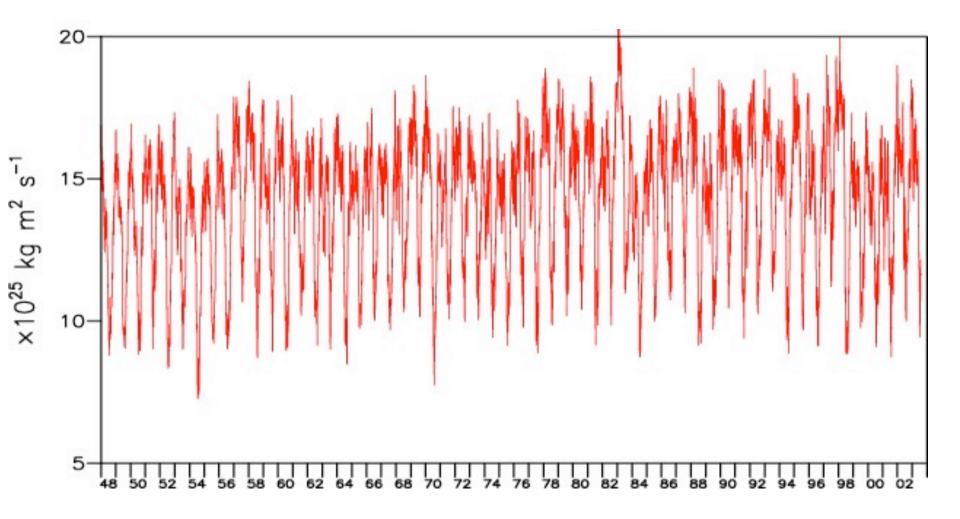


Filtered

Courtesy of David Salstein



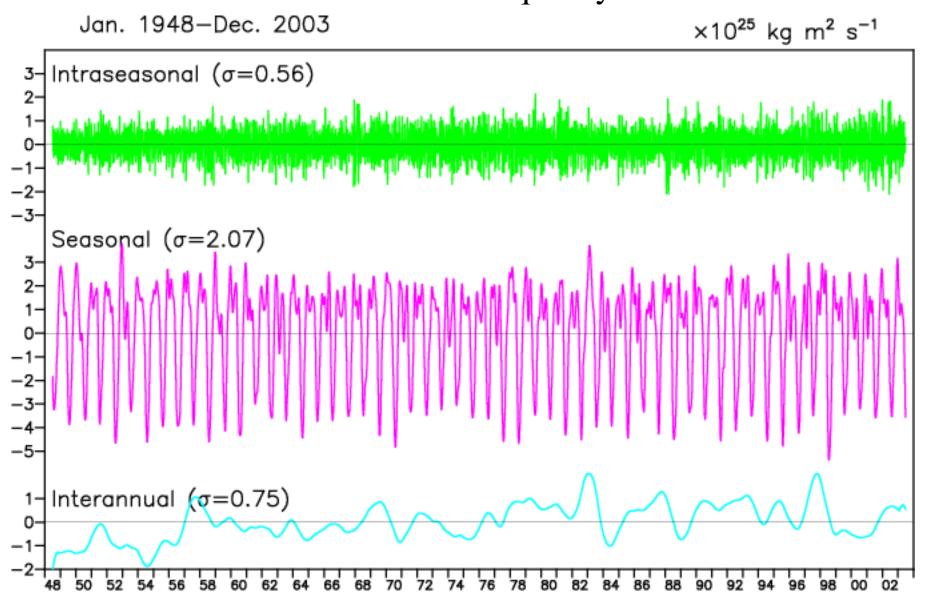
NCEP/NCAR Reanalysis AAM



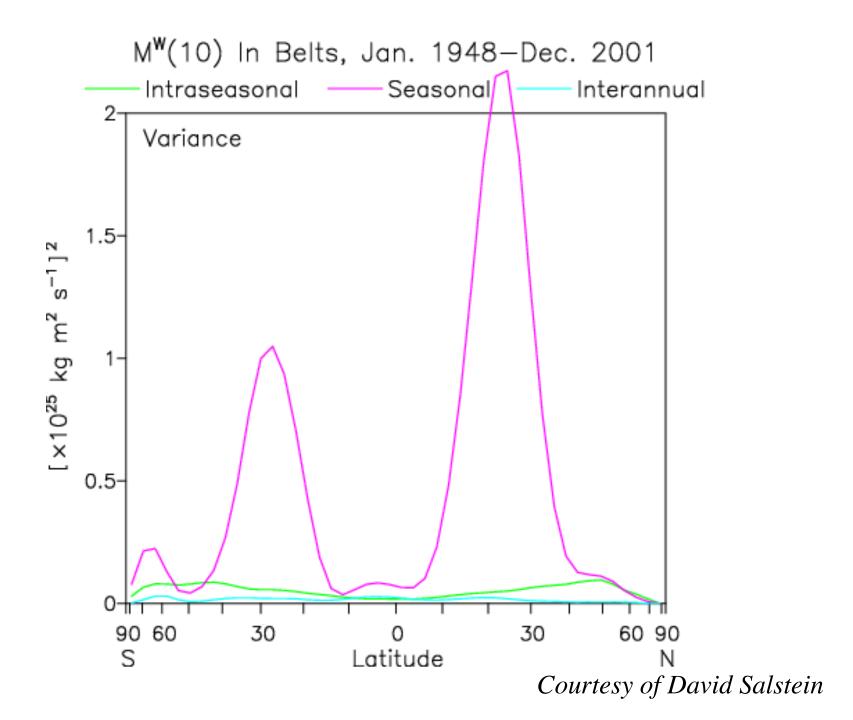
Note large seasonal cycle in angular momentum: factor of 2 between Jan/Feb and Jul/Aug

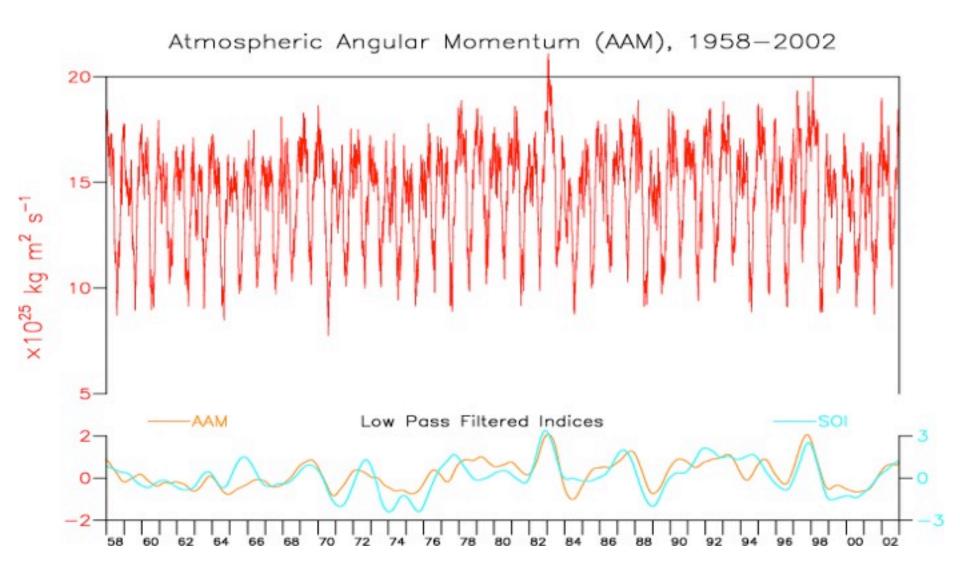
Courtesy of David Salstein

Breakdown into frequency bands



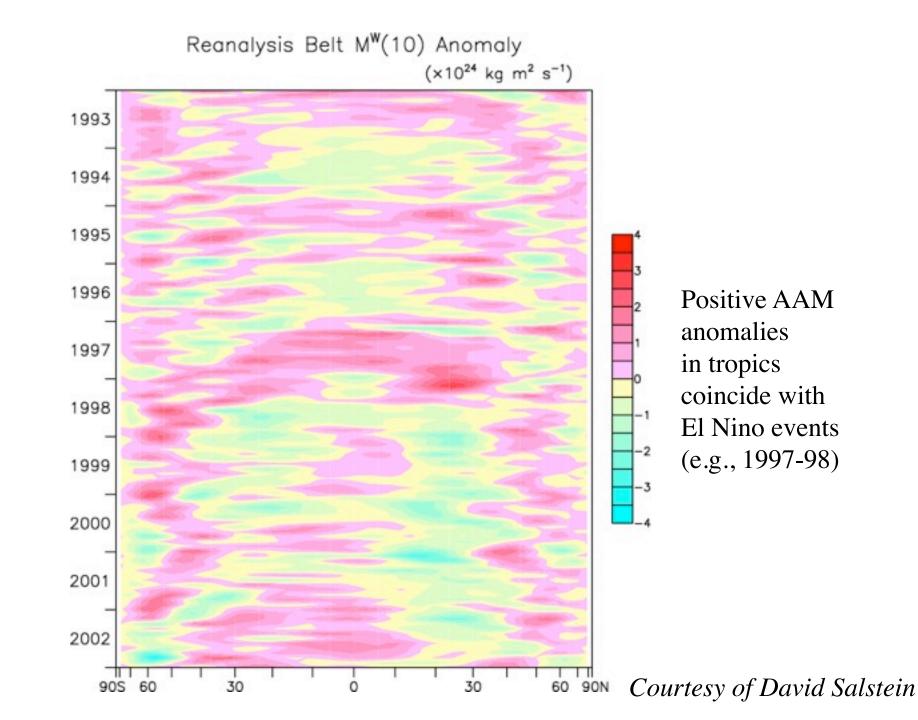
Courtesy of David Salstein





SOI = -Southern Oscillation Index; peaks correspond to El Nino events

Courtesy of David Salstein

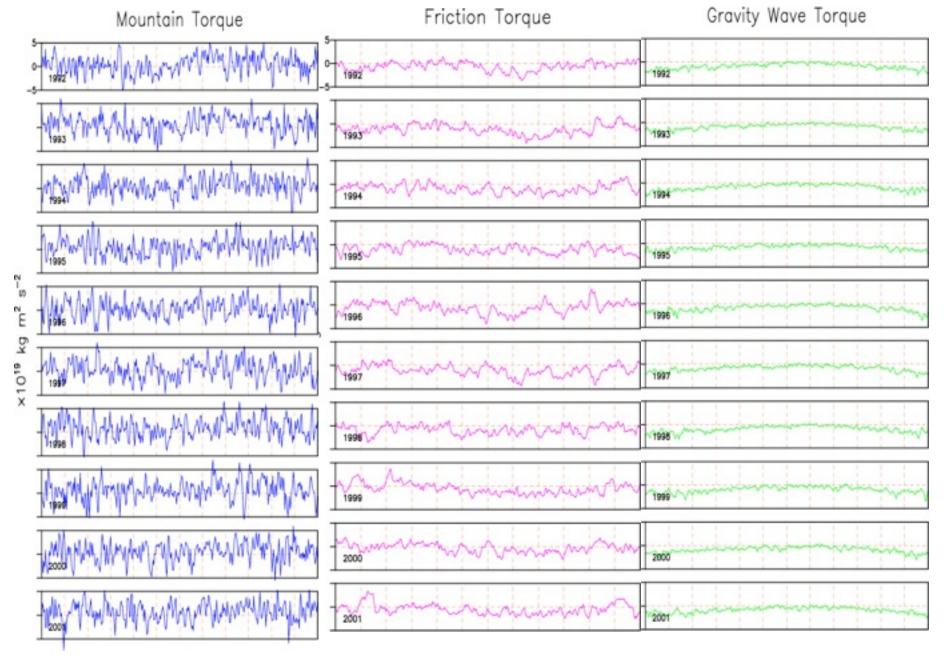


Mountain and friction torques

$$T_{mountain} = -R^2 \int \int p_s \frac{\partial H}{\partial \lambda} \cos \phi d\phi d\lambda$$

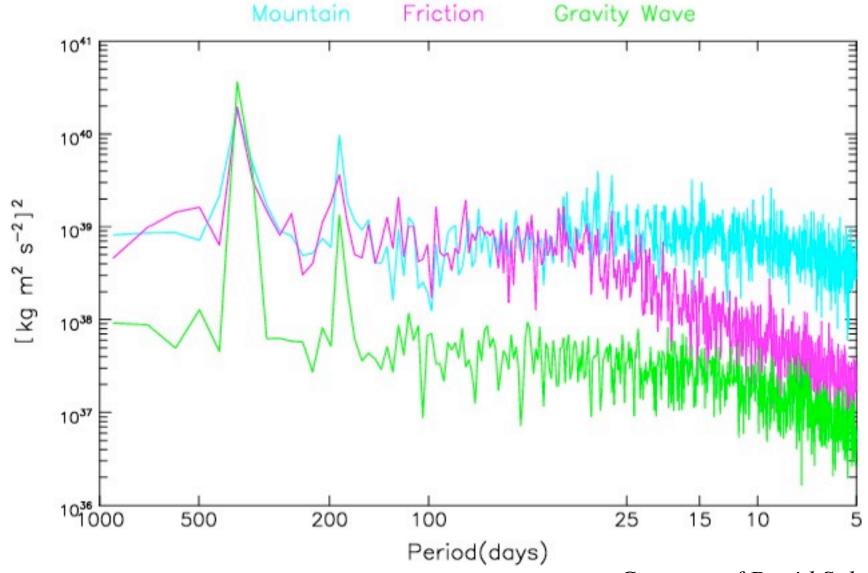
$$T_{friction} = R^3 \int \int \tau \cos^2 \phi d\phi d\lambda$$

R=Earth radius, \mathbf{p}_s =surface pressure, \mathbf{H} =topographic height τ =frictional stress, related to winds and roughness (model) ϕ =longitude λ =latitude *Courtesy of David Salstein*



Courtesy of David Salstein

NCEP Reanalysis Torques Power Spectra (1958-2002)



Courtesy of David Salstein

Regional Sources of Mountain Torque Variability and High-Frequency Fluctuations in Atmospheric Angular Momentum

HAIG ISKENDERIAN AND DAVID A. SALSTEIN

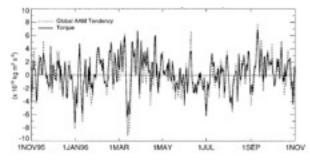
MONTHLY WEATHER REVIEW

VOLUME 126

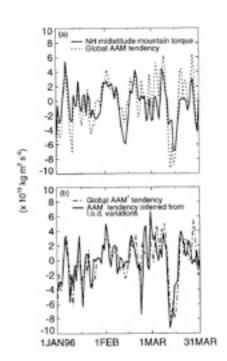
Surface Pressure Difference

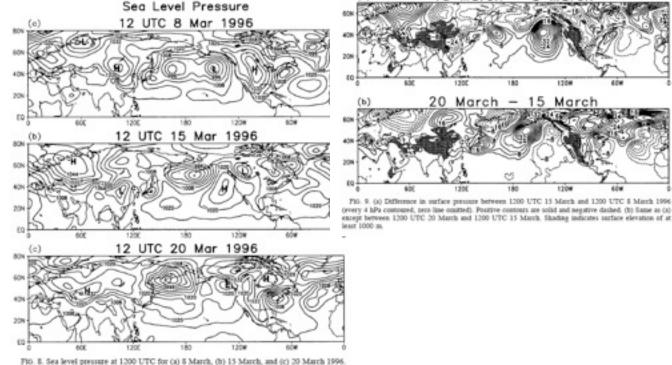
15 March - 8 March

20 March - 15 March

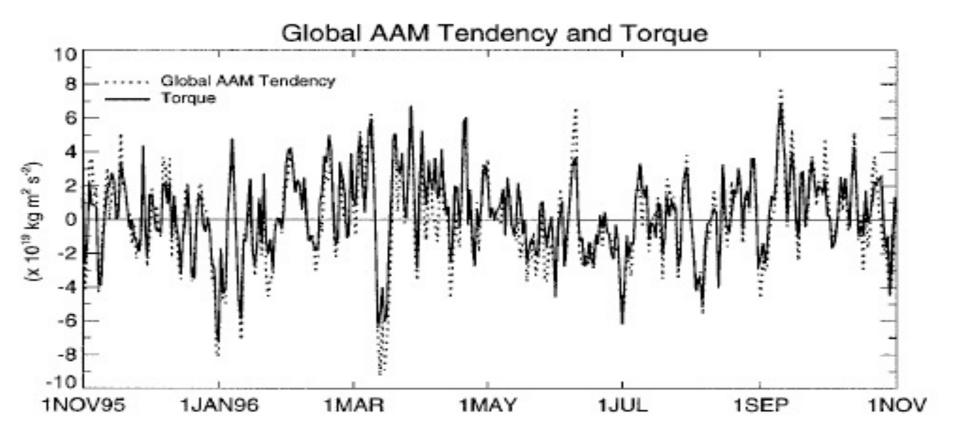


1682

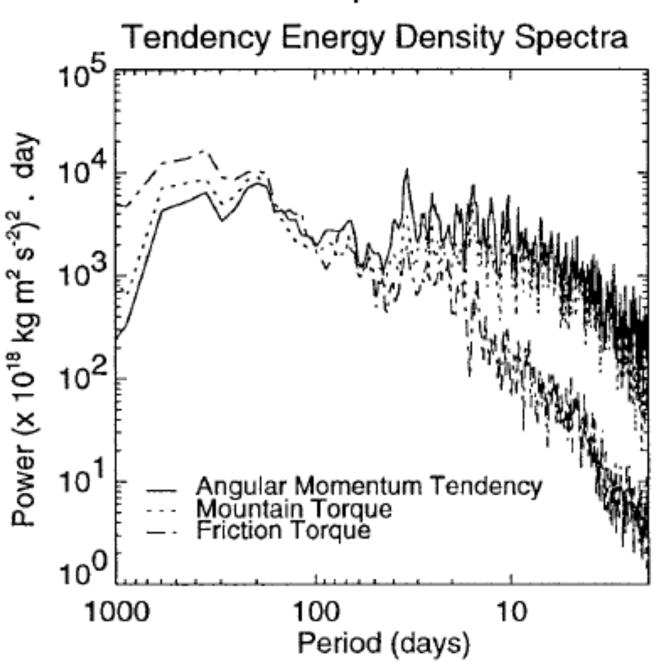


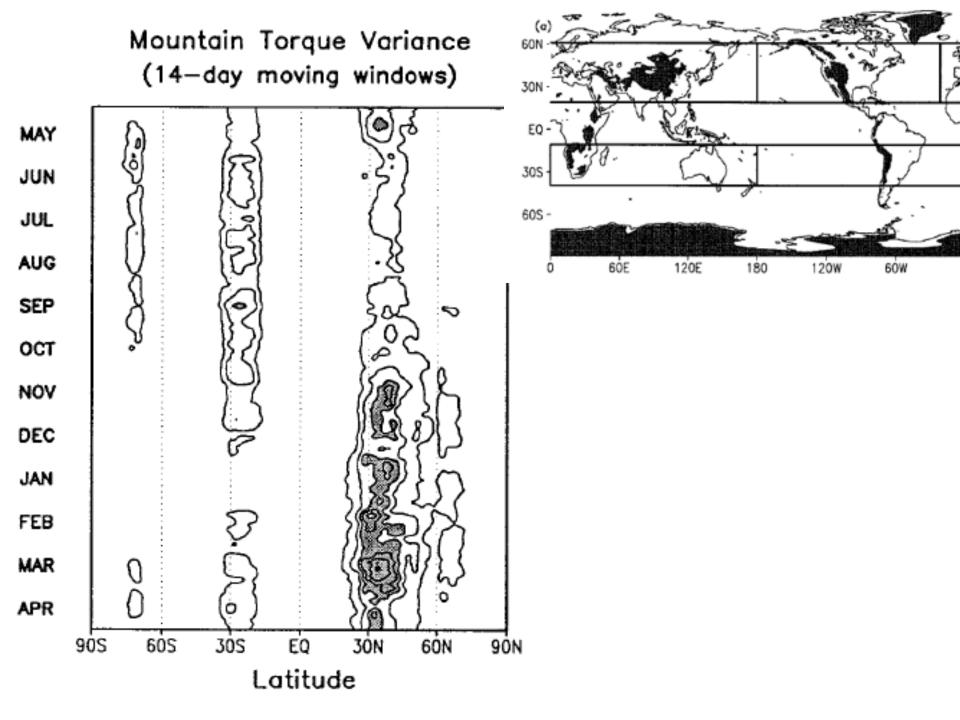


Contours are every 6 hPs. Highs and lows discussed in the text are indicated by the letters H



Global Torques and AAM





Surface Pressure Difference 15 March March (a) 60N 40N 20N ΕQ 120W 60E 120E 180 60W 20 March 15 March (b) 60N 40N

FIG. 9. (a) Difference in surface pressure between 1200 UTC 15 March and 1200 UTC 8 March 1996 (every 4 hPa contoured, zero line omitted). Positive contours are solid and negative dashed. (b) Same as (a) except between 1200 UTC 20 March and 1200 UTC 15 March. Shading indicates surface elevation of at least 1000 m.

180

120E

120W

60W

20N

EQ.

60E

November to April

For steady state: Integrated over the globe Net torque on atmosphere = 0

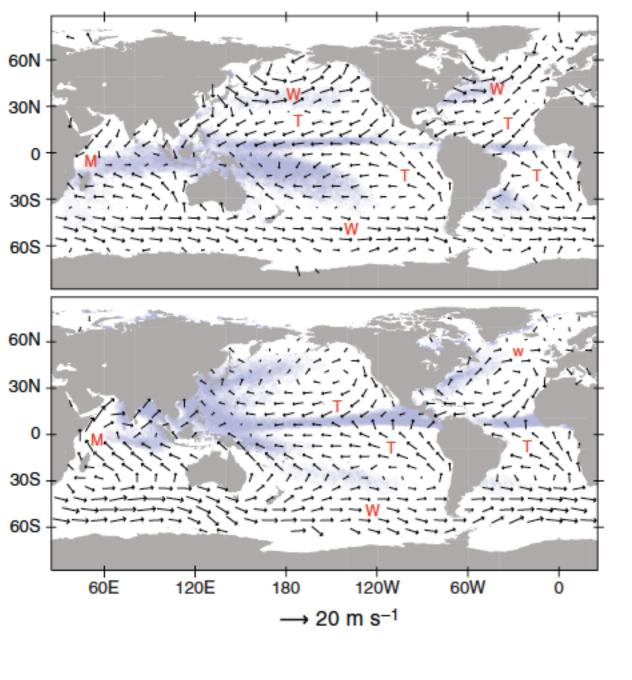
In the absence of mountains net frictional torque = 0

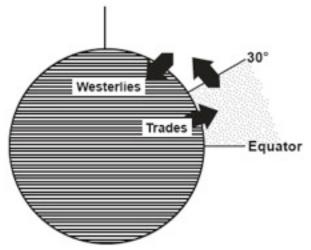
if the surface winds are nonzero, there must be regions of easterlies and westerlies For steady state: Integrated over the globe Net torque on atmosphere = 0

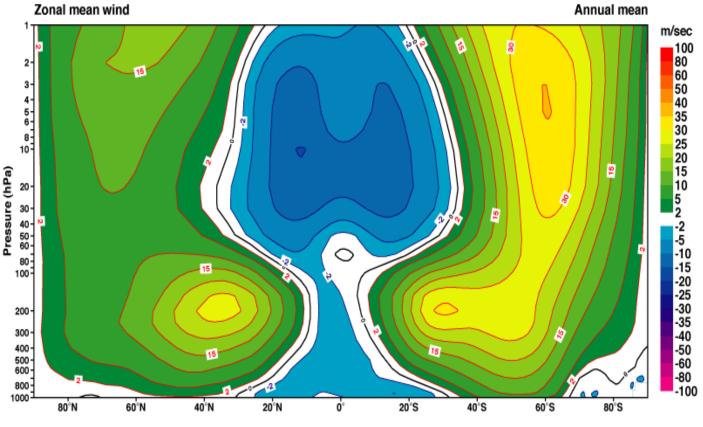
Hadley

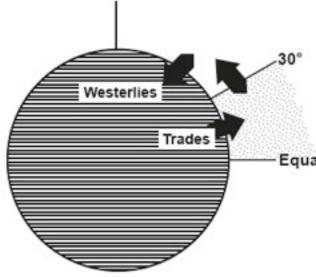
In the absence of mountains net frictional torque = 0

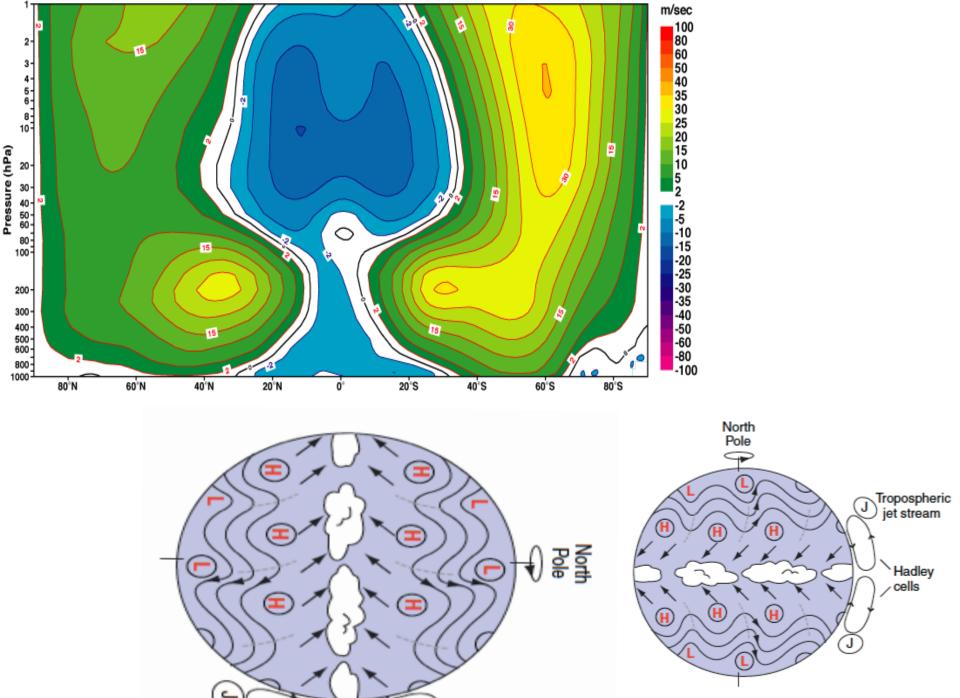
if the surface winds are nonzero, there must be regions of easterlies and westerlies











Annual mean

Zonal mean wind

$$-2\pi R_E^3 \int_{eq}^{30^\circ} \left[\overline{\tau_x} \right] \cos^2 \phi d\phi = \frac{2\pi R_E \cos \phi}{g} \int_{30^\circ} \left[\overline{mv} \right] dp$$

Torque equatorward of $30 = \text{Transport across } 30^{\circ}$

Another balance requirement:

$$-2\pi R_E^3 \int_{eq}^{30^\circ} \left[\overline{\tau_x} \right] \cos^2 \phi d\phi = \frac{2\pi R_E \cos \phi}{g} \int_{30^\circ} \left[\overline{mv} \right] dp$$

Torque equatorward of 30 = Transport across 30°

Poleward flux of AAM across 30° latitude in both hemispheres

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Torque equatorward of 30 = Transport across 30°

Poleward flux of AAM across 30° latitude in both hemispheres

$$\frac{2\pi R_E\cos\phi}{g}\int_{30^\circ}\left[\overline{mv}\right]dp = \frac{2\pi\Omega R_E^3\cos^3\phi}{g}\int_{30^\circ}\left[\overline{v}\right]dxdp + \frac{2\pi R_E^2\cos^2\phi}{g}\int_{30^\circ}\left[\overline{uv}\right]dxdp$$

Total

 M_{Ω}

 M_r

requires poleward mass flux

Decomposition of M_r

$$\left[\overline{uv}\right] = \left[\overline{u}\right]\left[\overline{v}\right] + \left[\overline{u'}\left[v\right]' + \left[\overline{u^*v^*}\right] + \left[\overline{u^{*'}v^{*'}}\right]$$

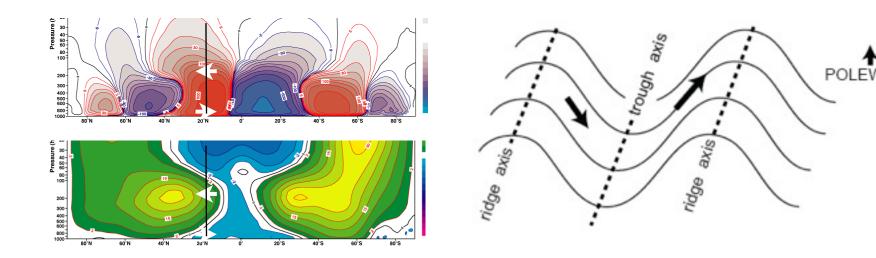
Steady MMC transient MMC

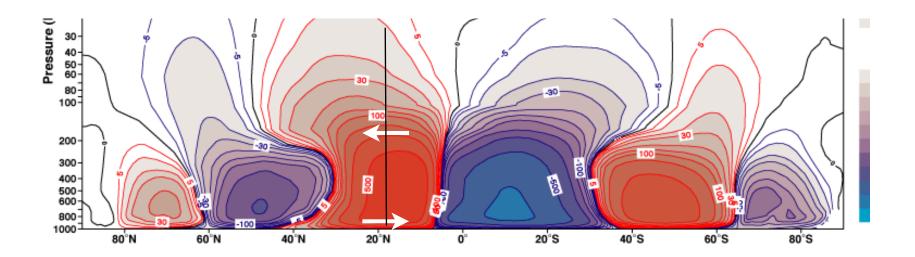
steady eddy transient eddy

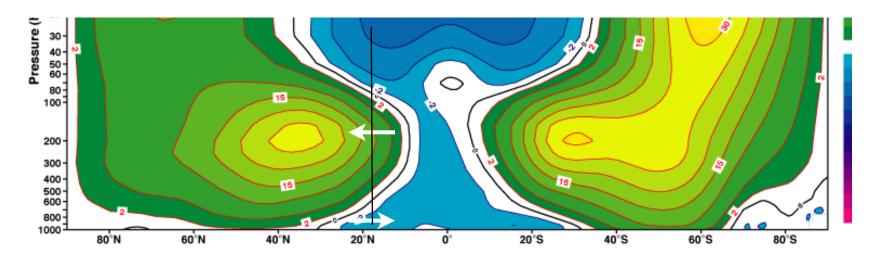
a.k.a. stationary wave

Decomposition of M_r

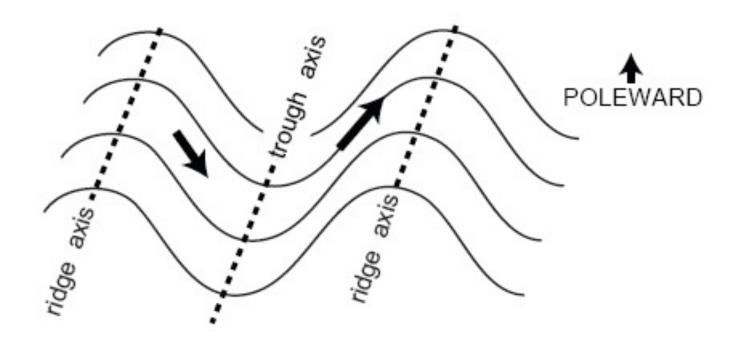
$$\left[\overline{uv}\right] = \left[\overline{u}\right]\left[\overline{v}\right] + \left[\overline{u'}\left[v\right]' + \left[\overline{u^*}\overline{v^*}\right] + \left[\overline{u^{*'}v^{*'}}\right]$$



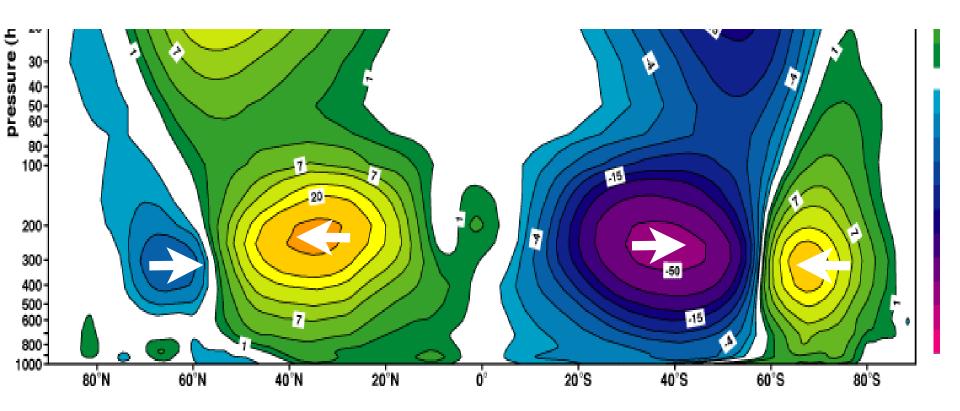


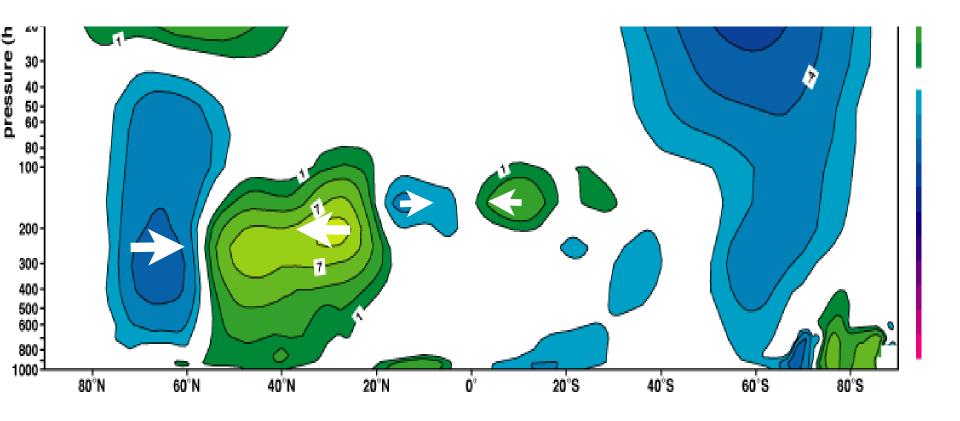


$$\int_0^{p_0} [u][v]dp$$

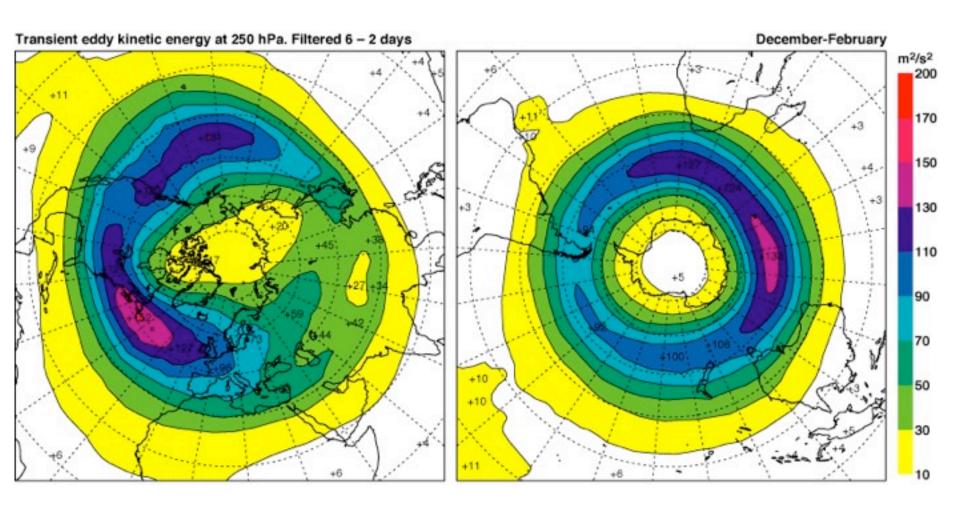


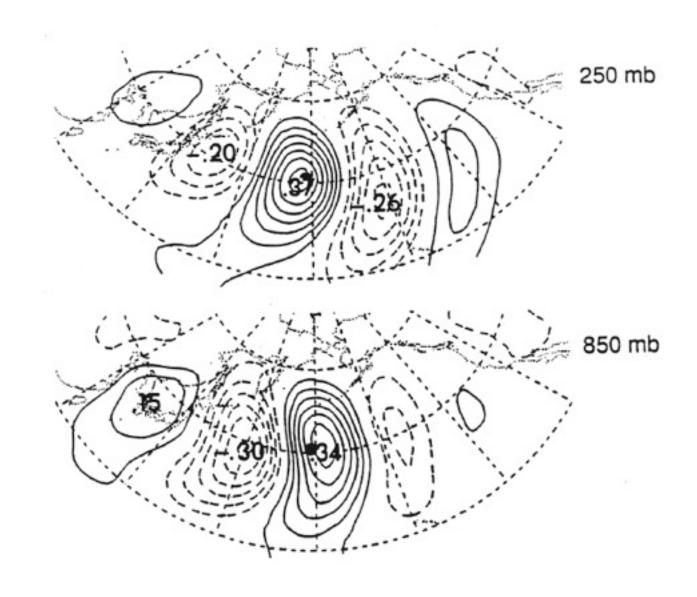
[u*v*]





Geopotential height at 500 hPa **December-February** 5600-





one-point correlation maps; 500 hPa height; highpass filtered

Conclusions

- In accordance with the balance requirements, there is a strong poleward flux of angular momentum across 30° latitude
- The flux is greater during winter when the surface westerlies are stronger
- The poleward flux across 30° is accomplished exclusively by the eddies
- Transient eddies and stationary waves both contribute
- Nearly all the flux occurs around the jet stream level (above 500 hPa)
- Balance requirement for an upward flox of M equatorward of 30° and a downward flux poleward of 30°

Vertical transport of angular momentum

$$rac{2\pi\Omega R_E^3}{g}\int-\left[\overline{\omega}
ight]\cos^3\phi dy+rac{2\pi R_E^2}{g}\int-\left[\overline{u}\overline{\omega}
ight]\cos^2\phi dy$$
 M_Ω

$$\frac{2\pi R_E^2}{g} \int -\left[\overline{\omega}\right] \left(\Omega R_E \cos\phi + \left[\overline{u}\right]\right) \cos^2\phi dy + \frac{2\pi R_E^2}{g} \int \left[\overline{u^*\omega^*}\right] \cos^2\phi dp$$

MMC term

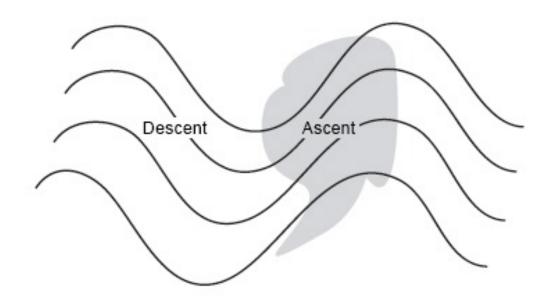
Eddy term

The eddies are not the answer

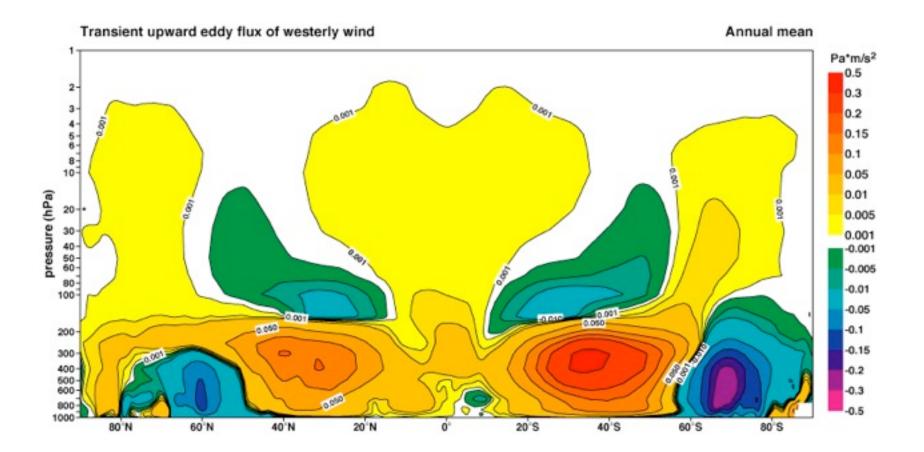
Scaling arguments: extratropical eddy fluxes are too small by a factor of *Ro*

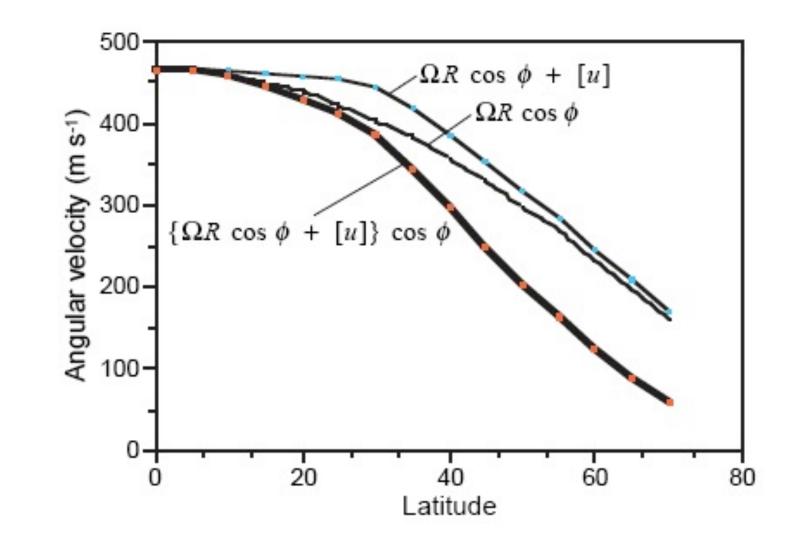
Tropical eddy fluxes are almost nonexistent

Extratropical eddy fluxes are upward; not downward



So it must be the MMC





"Spin down" of the circulation in a teacup

The zonally averaged equation of motion

Spherical geometry

$$\frac{\partial \left[u\right]}{\partial t} = \left[v\right] \left(f - \frac{1}{\cos\phi} \frac{\partial}{\partial y} \left[u\right] \cos\phi\right) - \left[\omega\right] \frac{\partial \left[u\right]}{\partial p} - \frac{1}{\cos^2\phi} \frac{\partial}{\partial \phi} \left[u^*v^*\right] \cos^2\phi - \frac{\partial}{\partial p} \left[u^*\omega^*\right] + F_x$$

Cartesian geometry

$$\frac{\partial \left[u\right]}{\partial t} = \left[v\right] \left(f - \frac{\partial \left[u\right]}{\partial y}\right) - \left[\omega\right] \frac{\partial \left[u\right]}{\partial p} - \frac{\partial}{\partial y} \left[u^* v^*\right] - \frac{\partial}{\partial p} \left[u^* \omega^*\right] + F_x$$

Neglecting vertical advection by MMC; using G to represent eddies

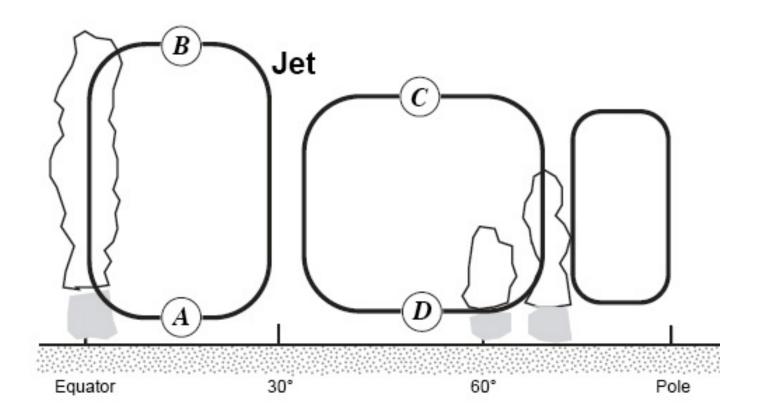
$$\frac{\partial \left[u\right]}{\partial t} = \left[v\right] \left(f - \frac{\partial \left[u\right]}{\partial y}\right) + G + F_x$$

$$\frac{\partial \left[u\right]}{\partial t} = \left[v\right] \left(f - \frac{\partial \left[u\right]}{\partial y}\right) + G + F_x$$

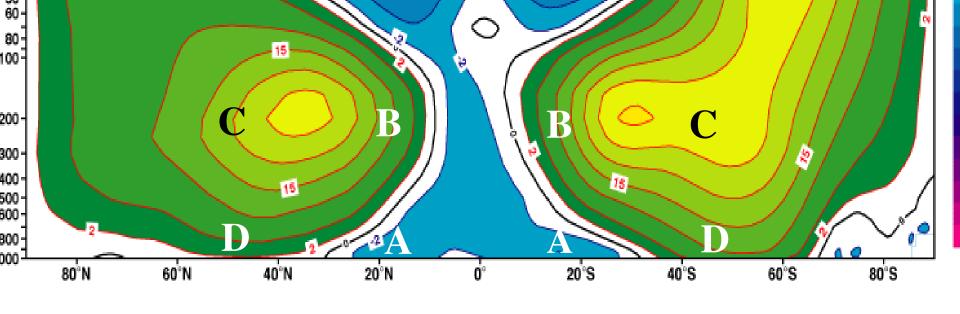
MMC dynamic stability eddy frictional $\propto dM/dy$ forcing drag

For long term "balance requirement" d/dt = 0

$$[v] = \frac{G + F_x}{f - \partial [u] / \partial y}$$



at A and D G = 0at B and C F = 0



at B $d[u]/dy \sim 30 \text{ m s}^{-1} \text{ over } 2000 \text{ km} \sim 1.5 \times 10^{-5} \text{s}^{-1}$

$$f \sim 4 \times 10^{-5} \text{s}^{-1}$$

 $f - d[u]/dy \sim 2.5 \times 10^{-5} \text{s}^{-1}$

at C $f - d[u]/dy \sim 10 \times 10^{-5} \text{s}^{-1}$

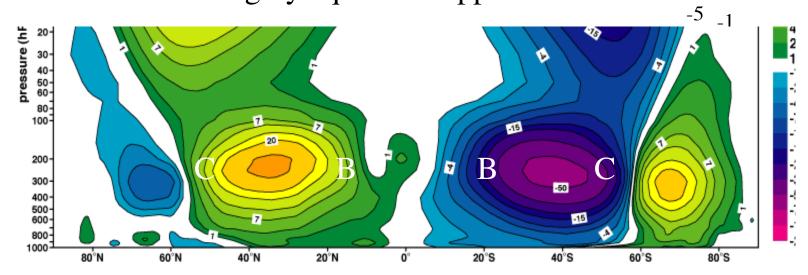
 $4 \times larger than at B$

Recalling that

$$[v] = \frac{G + F_x}{f - \partial [u] / \partial y}$$

and $F_x = 0$ at B and C

and G is roughly equal and opposite at B and C



Recalling that

$$[v] = \frac{G + F_x}{f - \partial [u] / \partial y}$$

and
$$F_r = 0$$
 at B and C

and G is roughly comparable at B and C

it follows that [v] is $\sim 4 \times$ stronger at B than at C i.e., that the Hadley cell is roughly 4 times as strong as the Ferrell cell

