

For low Ro flow $[f] \ll f$, and $f \approx f_g$, the interior flow satisfies

$$\left(\frac{d\eta}{dt}\right)_E = -\frac{f\partial}{2h}\eta = -\frac{f}{\tau_E}$$

i.e. there is an Ekman spindown timescale $\tau_E = \frac{2}{f}\left(\frac{h}{d}\right)$ associated with Ekman pumping.

Atm: $h = 10 \text{ km}$

$$d = 200 \text{ m} - 1 \text{ km} \Rightarrow \tau_E = 2 \times (10^{-5}) \times (10^4 \text{ s}) = 2-10 \text{ days}$$

Ocean

$h = 1 \text{ km}$

$$d = 5-30 \text{ m} \Rightarrow \tau_E = 2 \times (30-200) \times (10^4 \text{ s}) = 6-40 \text{ days}$$

Top Ekman Layer

$$-f(v - v_g) = \nu \frac{d^2 u}{dz^2}$$

$$f(u - u_g) = \nu \frac{d^2 v}{dz^2}$$

$$(u, v) \rightarrow (u_g, v_g) \text{ as } z \rightarrow -\infty$$

$$\rho \nu \frac{d\vec{u}}{dz} = \vec{\tau} \text{ at } z=0$$



Very similar to before. If $\vec{\tau} = \tau^x \hat{i} + \tau^y \hat{j}$, $\vec{s} = s_0 e^{(1+i)z/d} \Rightarrow \frac{\tau}{\rho \nu} = \left(\frac{ds}{dz}\right)_0 = \frac{s_0}{d}(1+i)$

$$u = u_g + \frac{2^{1/2}}{\rho f d} e^{z/d} \left\{ \tau^x \cos\left(\frac{z}{d} - \frac{\pi}{4}\right) - \tau^y \sin\left(\frac{z}{d} - \frac{\pi}{4}\right) \right\}$$

$$v = v_g + \frac{2^{1/2}}{\rho f d} e^{z/d} \left\{ \tau^x \sin\left(\frac{z}{d} - \frac{\pi}{4}\right) + \tau^y \cos\left(\frac{z}{d} - \frac{\pi}{4}\right) \right\} = \frac{2^{1/2}}{\rho f d} \left\{ \tau^x + i \tau^y \right\} \left\{ \cos \frac{\pi}{4} - i \sin \frac{\pi}{4} \right\}$$

$$\vec{M}_E = \int_{-\infty}^0 \rho (\vec{u} - \vec{u}_g) dz = \frac{1}{f} (\tau^y, -\tau^x) = \frac{1}{f} \hat{k} \times \vec{\tau} \quad (\text{so } f \hat{k} \times \vec{M}_E = -\vec{\tau} \text{ as before})$$



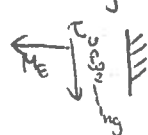
Ocean Ekman transport equal and opposite to atmosphere.

Note that $\nabla \cdot \vec{M}_E = \frac{1}{f} \left(\frac{\partial}{\partial x} \tau_y - \frac{\partial}{\partial y} \tau_x \right) = \frac{1}{f} \hat{k} \cdot \nabla \times \vec{\tau}$. This again produces Ekman pumping:

downwelling ($w_E < 0$)

upwelling ($w_E > 0$)

$$V \sim 10^3 \text{ m/s}$$



upwelling...equator

Magnitudes:

$$\tau_0 = 0.1 \text{ Pa}, \tau_0 = 10^{-4} \text{ Pa}, h = 20 \text{ m}, \Rightarrow M_E = \frac{\tau_0}{f} = 10^3 \frac{\text{kg}}{\text{m} \cdot \text{s}}$$

$$\Rightarrow v_E = \frac{M_E}{\rho \eta h} \sim \frac{10^3}{(10^3)(60)} \sim 1.5 \frac{\text{cm}}{\text{s}}$$

Integrated across the $W = 10^7 \text{ km} = 10^7 \text{ m}$

$$\Rightarrow M_E \cdot W = 10^{10} \frac{\text{kg}}{\text{s}} = 10 \text{ Sv}$$

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Thus, for midocephalyres where $\gamma \ll f$,

Since $\frac{df}{dt} = v \frac{df}{dy} = \beta v$,

... responsible for most of the upper-ocean currents.

$$\Delta \tau = \frac{\Delta x}{c} = \frac{0.1 \text{ Pa} \frac{\text{kg}}{\text{m} \cdot \text{s}}}{2000 \times 10^3 \text{ m}} \sim 0.5 \times 10^{-7} \frac{\text{kg}}{\text{m}^2 \cdot \text{s}}$$

$$\Rightarrow V = \frac{1}{ph\beta} \Delta x \tau = \frac{0.5 \times 10^{-7}}{(\frac{10}{m})(10^{-3} m)(15 \times 10^{-11} s)}$$

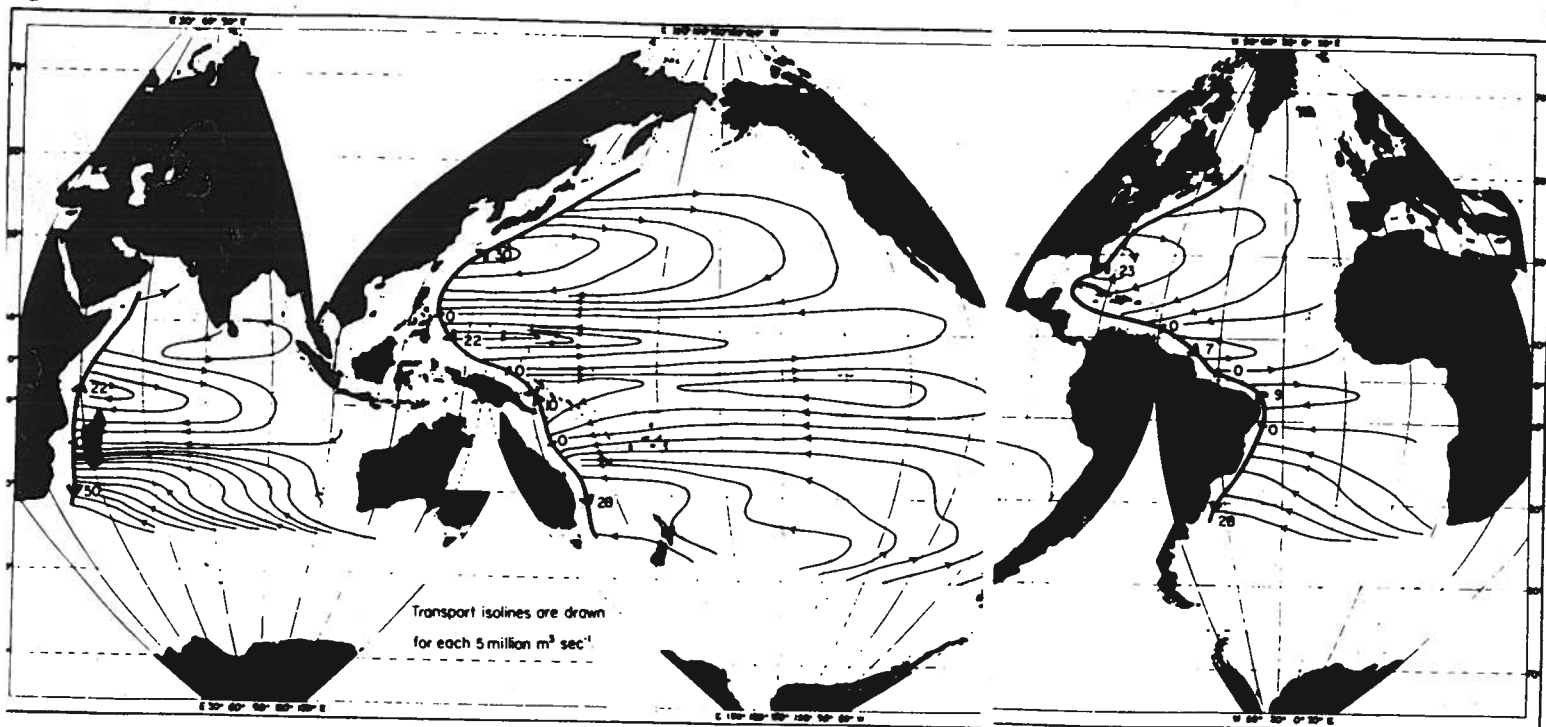
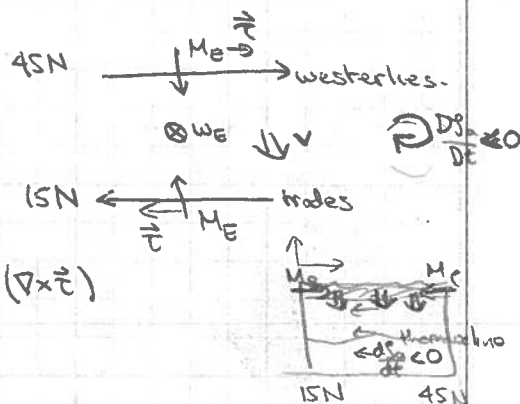


Figure 5.3.4 The Sverdrup transport and the implied western boundary currents in the oceans corresponding to the annual mean wind-stress field. The Sverdrup transport is required to satisfy the normal-flow condition on oceanic eastern boundaries. Figures represent the volume transports in $10^6 \text{ m}^3 \text{ s}^{-1}$. (Reprinted courtesy Welander, 1959.)

Real Geophysical Ekman Layers

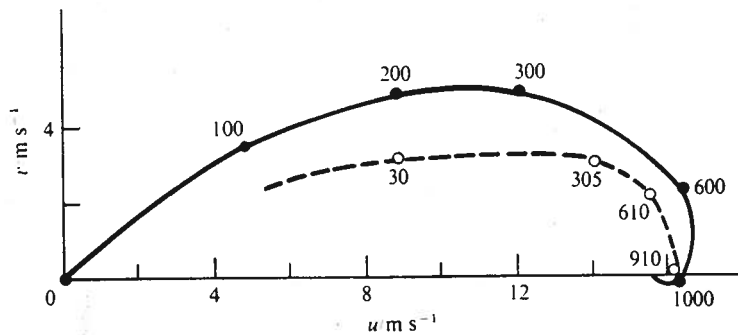
AtmosphereTurbulence

Fig. 9.2. Wind hodograph for the lowest kilometre as measured by Dobson (1914) (dashed line) compared with Ekman spiral (full line). Figures on curves are heights in metres.

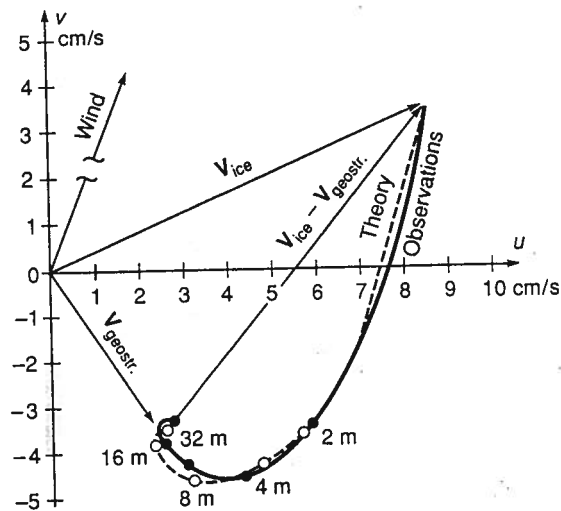
Ocean

Figure 5-7 Comparison between observed currents below a drifting ice floe at 84.3°N and theoretical predictions based on an eddy viscosity $\nu = 2.4 \times 10^{-3} \text{ m}^2/\text{s}$. (Reprinted from *Deep-Sea Research*, 13, Kenneth Hunkins, Ekman drift currents in the Arctic Ocean, p. 614, copyright 1966, with kind permission from Pergamon Press Ltd, Headington Hill Hall, Oxford OX3 0BW, UK.)